

Safety Evaluation of Flashing Beacons at STOP-Controlled Intersections

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FOREWORD

The goal of this research was to evaluate and estimate the effectiveness of flashing beacons at stop-controlled intersections as one of the strategies in the Evaluation of Low-Cost Safety Improvements Pooled Fund Study (ELCSI-PFS), Phase I.

This research provides Crash Reduction Factor (CRF) and economic analysis for the effectiveness of flashing beacons at stop controlled intersections strategy. The estimate of effectiveness for flashing beacons at stop-controlled intersections strategy was determined by conducting scientifically rigorous before-after evaluations at sites where this strategy was implemented in the United States.

The above safety improvement and all other targeted strategies in the ELCSI-PFS are identified as low-cost strategies in the *NCHRP Report 500* guidebooks. Participating States in the ELCSI-PFS are Arizona, California, Connecticut, Florida, Georgia, Illinois, Indiana, Iowa, Kansas, Kentucky, Maryland, Massachusetts, Minnesota, Mississippi, Montana, New York, North Carolina, North Dakota, Oklahoma, Pennsylvania, South Carolina, South Dakota, Tennessee, Texas, Utah, and Virginia.

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SI* (MODERN METRIC) CONVERSION FACTORS

APPROXIMATE CONVERSIONS TO SI UNITS

Symbol	When You Know	Multiply By	To Find	Symbol
LENGTH				
in	inches	25.4	millimeters	mm
ft	feet	0.305	meters	m
yd	yards	0.914	meters	m
mi	miles	1.61	kilometers	km
AREA				
in ²	square inches	645.2	square millimeters	mm ²
ft ²	square feet	0.093	square meters	m ²
yd ²	square yard	0.836	square meters	m ²
ac	acres	0.405	hectares	ha
mi ²	square miles	2.59	square kilometers	km ²
VOLUME				
fl oz	fluid ounces	29.57	milliliters	mL
gal	gallons	3.785	liters	L
ft ³	cubic feet	0.028	cubic meters	m ³
yd ³	cubic yards	0.765	cubic meters	m ³
NOTE: volumes greater than 1000 L shall be shown in m ³				
MASS				
oz	ounces	28.35	grams	g
lb	pounds	0.454	kilograms	kg
T	short tons (2000 lb)	0.907	megagrams (or "metric ton")	Mg (or "t")
TEMPERATURE (exact degrees)				
°F	Fahrenheit	5 (F-32)/9 or (F-32)/1.8	Celsius	°C
ILLUMINATION				
fc	foot-candles	10.76	lux	lx
fl	foot-Lamberts	3.426	candela/m ²	cd/m ²
FORCE and PRESSURE or STRESS				
lbf	poundforce	4.45	newtons	N
lbf/in ²	poundforce per square inch	6.89	kilopascals	kPa

APPROXIMATE CONVERSIONS FROM SI UNITS

Symbol	When You Know	Multiply By	To Find	Symbol
LENGTH				
mm	millimeters	0.039	inches	in
m	meters	3.28	feet	ft
m	meters	1.09	yards	yd
km	kilometers	0.621	miles	mi
AREA				
mm ²	square millimeters	0.0016	square inches	in ²
m ²	square meters	10.764	square feet	ft ²
m ²	square meters	1.195	square yards	yd ²
ha	hectares	2.47	acres	ac
km ²	square kilometers	0.386	square miles	mi ²
VOLUME				
mL	milliliters	0.034	fluid ounces	fl oz
L	liters	0.264	gallons	gal
m ³	cubic meters	35.314	cubic feet	ft ³
m ³	cubic meters	1.307	cubic yards	yd ³
MASS				
g	grams	0.035	ounces	oz
kg	kilograms	2.202	pounds	lb
Mg (or "t")	megagrams (or "metric ton")	1.103	short tons (2000 lb)	T
TEMPERATURE (exact degrees)				
°C	Celsius	1.8C+32	Fahrenheit	°F
ILLUMINATION				
lx	lux	0.0929	foot-candles	fc
cd/m ²	candela/m ²	0.2919	foot-Lamberts	fl
FORCE and PRESSURE or STRESS				
N	newtons	0.225	poundforce	lbf
kPa	kilopascals	0.145	poundforce per square inch	lbf/in ²

*SI is the symbol for the International System of Units. Appropriate rounding should be made to comply with Section 4 of ASTM E380. (Revised March 2003)

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ABBREVIATIONS AND SYMBOLS

Abbreviations

A	Injury, incapacitating
AADT	Average annual daily traffic
AASHTO	American Association of State Highway Transportation Officials
B	Injury, nonincapacitating
C	Possible injury
EB	Empirical Bayes
EPDO	Equivalent property damage only
FHWA	Federal Highway Administration
GOF	Goodness-of-fit
HPMS	Highway Performance Monitoring System
HSIS	Highway Safety Information System
KABCO	Scale used to represent injury severity in crash reporting
K	Fatality
MUTCD	Manual Uniform Traffic Control Devices
NC	North Carolina
NCDOT	North Carolina Department of Transportation
NCHRP	National Cooperative Highway Research Program
NHTSA	National Highway Traffic Safety Administration
O	Property damage only
PDO	Property damage only
R-square (FT)	Freeman Tukey R-square
SAS	Statistical Analysis Software
SC	South Carolina
SCDOT	South Carolina Department of Transportation
S.E.	Standard Error
SPF	Safety performance functions
TEAAS	Traffic Engineering Accident Analysis
TRB	Transportation Research Board

Symbols

α	Greek letter Alpha
β	Greek letter Beta
Δ	Greel letter Delta
λ	Greek letter Lamda
π	Greek letter Pi
θ	Greek letter Theta

EXECUTIVE SUMMARY

The Federal Highway Administration (FHWA) organized a pooled fund study of 26 States to evaluate low-cost safety strategies as part of its strategic highway safety effort. The purpose of the FHWA Low-Cost Safety Improvements Pooled Fund Study is to evaluate the safety effectiveness of several of the low-cost strategies through scientifically rigorous crash-based studies. One of the strategies chosen to be evaluated for this study was flashing beacons at stop-controlled intersections. This strategy is intended to reduce the frequency of crashes related to drivers' lack of awareness of stop control at unsignalized intersections. The safety effectiveness of this strategy had not previously been documented. This study is an attempt to provide an evaluation through scientifically rigorous procedures. Three types of flashing beacons—intersection control beacons, beacons mounted on STOP signs, and actuated beacons—were considered collectively at stop-controlled intersections. Although these could be considered three distinct safety strategies with different expected performance, because of sample size limitations, they were analyzed collectively in this study.

Geometric, traffic, and crash data were obtained at stop-controlled intersections for 64 sites in North Carolina and 42 sites in South Carolina. These States were selected for the study because they had information about the location of these treatments and when these treatments were installed. In both States, sites were selected for this treatment because of a large number of angle crashes involving drivers who had difficulty in recognizing the stop control condition. Empirical Bayes methods were incorporated in a before-after analysis to determine the safety effectiveness of installing flashing beacons, while accounting for potential selection bias and the resulting regression-to-the-mean effects. Overall, installation of flashing beacons in North Carolina resulted in a statistically significant reduction in total crashes, angle crashes, and injury and fatal crashes. The intersections in South Carolina experienced very little change following the introduction of flashing beacons. The combined results from both the States indicate a statistically significant reduction in angle crashes and injury and fatal crashes. From a practical standpoint, the aggregate analysis supports the conclusion that an angle crash reduction of 13 percent and an injury and fatal crash reduction of 10 percent can be expected with the installation of flashing beacons, based on the point estimate.

The economic analysis based on the combined results for angle and nonangle crashes from both States indicates that standard flashing beacons (those that flash continuously) and some of the actuated ones (i.e., the less expensive beacons) are economically justified, but that a benefit cost ratio of 2:1 may not be achievable for the more expensive actuated beacon types.

INTRODUCTION

Background on Strategy

Intersections account for a small portion of the total highway system, yet in 2005, approximately 2.5 million intersection-related crashes occurred, representing 41 percent of all reported crashes. Intersection-related crashes account for more than 50 percent of total crashes in urban areas and over 30 percent of total crashes in rural areas. Out of a total of 39,189 fatal crashes in 2005, 22 percent, or 8,655, occurred at or within an intersection environment.⁽¹⁾ The high frequency of crashes is not surprising, however, due to the fact that intersections present more points of conflict than nonintersections.

Unsignalized intersections often present potential hazards not associated with signalized intersections. A traffic signal provides distinct priority to specific movements; this priority can be less obvious at unsignalized intersections. This is often problematic on two-lane highways because of the priority of movement on the major roadway. The differences between signalized and unsignalized intersections are also associated with differences in crash types. Unsignalized intersections tend to experience more angle and turning collisions; signalized intersections experience more rear-end collisions.

Driver compliance with the intersection traffic control is vital to intersection safety. The typical location of unsignalized intersections, however, presents several challenges. Unsignalized intersections are usually located along low- to moderate-volume roads in rural and suburban areas that are generally associated with high-speed travel and relatively lower geometrics than those in more developed suburban and urban areas.⁽²⁾ Many unsignalized intersections may be unexpected or may not be visible to approaching drivers, particularly those drivers on the major road. Therefore, enhancing the visibility and conspicuity of unsignalized intersections has the potential to reduce the number of crashes associated with drivers' lack of awareness of the intersection.

Installing flashing beacons over the intersection or along the roadside can help alert drivers to the presence of an intersection. The *Manual on Uniform Traffic Control Devices* (MUTCD), Chapter 4K, defines flashing beacons as a highway traffic signal with one or more signal sections that operates in a flashing mode. It can provide traffic control when used as an intersection control beacon or warning in alternative uses.⁽³⁾

Flashing beacons may be particularly appropriate for unsignalized intersections with patterns of angle collisions related to lack of driver awareness of the intersection.⁽²⁾ Flashing beacons can be designed in such a way as to flash all the time or flash only when a sensor detects a vehicle approaching the intersection (an actuated beacon). Beacons can be installed either overhead, as shown in figure 1, or mounted directly on a STOP sign, as shown in figure 2. Some of the actuated overhead beacons are supplemented with a sign that indicates "Vehicles Entering When Flashing." The success of this strategy will rely on selecting an appropriate combination of markings for the specific conditions on the approaches to the intersection.



Figure 1. Photo. Example of Standard Overhead Flashing Beacon.



Figure 2. Photo. Example of a STOP Sign Mounted Flashing Beacon.

The flashing beacons discussed in this report can be classified into three groups:

- Intersection control beacons that are mounted over the intersection, referred to as “standard overhead beacons” in this report.
- STOP sign mounted flashing beacons, referred to as “standard STOP sign mounted beacons” in this report.
- Actuated flashing beacons including both those that are mounted over the intersection and mounted on signs, referred to as “actuated beacons” in this report.

Collectively, they are referred to in this report as flashing beacons.

Background on Study

In 1997, the American Association of State Highway and Transportation Officials (AASHTO) Standing Committee for Highway Traffic Safety, with the assistance of the FHWA, the National Highway Traffic Safety Administration (NHTSA), and the Transportation Research Board (TRB) Committee on Transportation Safety Management, met with safety experts in the field of driver, vehicle, and highway issues from various organizations to develop a strategic plan for highway safety. These participants developed 22 key areas that affect highway safety. One of these areas is unsignalized intersection crashes.

The National Cooperative Highway Research Program (NCHRP) published a series of guides to advance the implementation of countermeasures targeted to reduce accidents and injuries. Each guide addresses one of the 22 emphasis areas and includes an introduction to the problem, a list of objectives for improving safety in that emphasis area, and strategies for each objective. Each strategy is designated as “proven,” “tried,” or “experimental.” Many of the strategies discussed in these guides have not been rigorously evaluated; about 80 percent of the strategies are considered “tried” or “experimental.”

The FHWA organized a pooled fund of 26 States to study low-cost safety strategies as part of the strategic highway safety effort. The purpose of the Pooled Fund Study was to evaluate the safety effectiveness of several low-cost safety strategies, both tried and experimental, through scientifically rigorous crash-based studies. Based on inputs from the Pooled Fund Study Technical Advisory Committee and the availability of data, installing flashing beacons at unsignalized intersections was selected as a strategy that should be evaluated as part of this effort.

Literature Review

Very few studies have evaluated flashing beacons at stop-controlled intersections. Cribbins and Walton evaluated the safety impacts of flashing beacons at 14 rural intersections in North Carolina that were installed after 1965.⁽⁴⁾ They compared at least one year of crash data before the beacons were installed to at least one year of crash data after the installation of the beacons. Based on the severity level of each accident and the total number of vehicles entering the intersections, an equivalent property damage only (EPDO) rate was computed. The EPDO rate before the installation of the beacons was compared with the EPDO rate after the installation. Following the installation of the beacons, the EPDO rate decreased by 48 percent. Based on a paired *t*-test, the authors concluded that the reduction was statistically significant at the 0.01 level.

Pant et al. compared the crash rates at six stop-controlled intersections without a beacon to seven stop-controlled intersections with a beacon.⁽⁵⁾ Fatal, injury, property damage only (PDO), and right-angle crashes were included in the analysis. The mean rates for most accident types were higher at beacon-controlled intersections compared to stop-controlled intersections without a beacon. Considering that beacons may be installed at sites with higher than average crash rates, it is not surprising that beacon-controlled sites had a higher crash rate. A before-after analysis was completed for the seven beacon-controlled sites, which did not include any control sites. The frequency of fatal, serious visible injury, and angle accidents decreased following the installation

of beacons; however, none of these reductions were statistically significant based on a chi-square test.

More recently, Murphy and Hummer evaluated the safety impacts of flashing beacons at 34 locations in North Carolina.⁽⁶⁾ All of the locations were four-leg intersections with no turn lanes and two-way stop control. Three different methods were used to conduct the analysis: naïve before and after analysis, before and after analysis using a safety performance function, and the Empirical Bayes (EB) method. The naïve before and after analysis revealed a 10-percent reduction in total crashes, 15-percent reduction in injury crashes, 66-percent reduction in severe injury crashes, 11-percent reduction in frontal impact crashes, and a 50-percent reduction in ran STOP sign crashes. A safety performance function developed by Vogt and Bared⁽¹⁾ for intersections in Minnesota was recalibrated using data from 170 reference intersections in North Carolina. This method showed a 13-percent increase in total crashes following the introduction of flashing beacons. The EB approach was applied to account for potential effects of regression-to-the-mean. The EB approach also made use of data from the reference population, but accounted for the increase in traffic volume using a linear assumption. However, considering that the safety performance function used by the authors showed that the relationship between crash frequency and major and minor average annual daily traffic (AADT) is not linear, assuming a linear change will give an incorrect result. Their EB approach revealed a 12-percent decrease in total crashes, 9-percent decrease in injury crashes, 40-percent decrease in severe-injury crashes, 9-percent decrease in frontal-impact crashes, and 26-percent reduction in failure-to-stop crashes.

Based on the referenced studies, it can be concluded that the safety effectiveness of flashing beacons at stop-controlled intersections has not been adequately quantified. Two studies were based on a limited sample and did not apply state-of-the-art methods to account for potential effects of regression-to-the-mean. The third study attempted to use the EB method to account for regression-to-the-mean, but did not properly account for changes in traffic volume. It is clear that a thorough investigation is needed that will properly account for both regression-to-the-mean and changes in traffic volume is needed to evaluate the effectiveness of flashing beacons in reducing crash frequency and severity for different configurations of unsignalized intersections.

OBJECTIVE

The objective of this research was to examine the safety impact of flashing beacons at stop-controlled intersections. The expected change in crash frequency was estimated for several target crash types, including the following:

- Total intersection crashes.
- Total intersection injury and fatal crashes (including K, A, B, and C on KABCO scale).
- Total intersection angle crashes.
- Total intersection rear-end crashes.

A second objective was to examine the impact of these beacons on “total harm” expressed in terms of crash costs. Unit crash costs for different crash types and crash severity were based on a recent study conducted by FHWA.⁽⁸⁾

A further objective was to determine if the safety impacts are a function of:

- Area type (rural, suburban, or urban).
- Intersection type (two-way versus four-way stop-controlled).
- Types of flashing beacon installations (standard overhead, standard STOP sign mounted, and actuated).

Meeting these objectives placed some special requirements on the data collection and analysis tasks. These were:

- The need to select a large enough sample size to detect, with statistical significance, what may be small changes in safety for some crash types.
- The need to carefully select reference sites.
- The need to properly account for traffic volume changes.
- The need to pool data from multiple jurisdictions to improve reliability of the results and facilitate broader applicability of the products of the research.

STUDY DESIGN

The study design involved a sample size analysis and prescription of needed data elements. This was done to assess the sample size required to detect statistically an expected change in safety and also determine what changes in safety can be detected with likely available sample sizes.

Assumptions on the expected safety effects and on the crash frequency at potential strategy sites in the before period are basic to estimating sample sizes. Following a literature review, and the application of methodology in Hauer,⁽⁹⁾ a minimum sample size was estimated. This sample size analysis undertaken for this study addresses how large a sample is required to statistically detect an expected change in safety.

For this analysis, it was assumed at the time the study was designed that a conventional before-after study with reference group design would be used, since available sample size estimation methods are based on this assumption. To facilitate the analysis, it was also assumed that the number of reference sites is equal to the number of strategy sites. The sample size estimates provided would be conservative in that state-of-the-art EB methodology proposed for the evaluations would require fewer sites.

Sample sizes are estimated for various assumptions of likely safety effect and crash frequencies before the strategy was installed. Table 1 provides the crash rate assumptions used. Rate A is based on a Minnesota study.⁽¹⁰⁾ Rate B is based on an Ohio Study.⁽⁵⁾ Rate C is based on Minnesota data from a model validation study.⁽¹¹⁾ Right-angle and rear-end proportions were adopted from SafetyAnalyst data.⁽¹²⁾

Table 1. Before Period Crash Rate Assumptions.

Crash Type	Rate A (crashes/intersection/ year)	Rate B (crashes/intersection/ year)	Rate C (crashes/intersection/ year)
All	3.45	7.62	0.44
Right-Angle (39% of total assumed)	1.35	2.97	0.17
Rear-End (23% of total assumed)	0.79	1.75	0.10

Table 2 provides estimates of the required number of before period intersection-years in the sample for both the 90-percent and 95-percent confidence levels. The calculations assume equal number of intersection-years for strategy and comparison sites and equal length of before and after periods. Intersection-years is the number of intersections where the strategy was applied multiplied by the number of years the strategy was in place at each intersection. For example, if a strategy was applied at 9 intersections and has been in place for 3 years at all 9 intersections, this is 27 intersection-years.

A minimum sample size of 135 intersection-years and a desirable sample size of 260 intersection-years per period were calculated as shown in bold in table 2. It was expected that these sample sizes could be reduced if the assumption for crashes per intersection-year before strategy implementation turns out to be conservatively low for strategy data, or if more after period years than assumed are available. The desirable sample assumes that the reduction in crashes could be as low as a 10-percent reduction in all crashes and that this is the smallest benefit that one would be interested in detecting with 90-percent confidence. The logic behind this approach is that safety managers may not wish to implement a measure that reduces crashes by less than 10 percent, and the required sample size to detect a reduction smaller than 10 percent would likely be prohibitively large. The minimum sample indicates the level for which a study seems worthwhile (i.e., it is feasible to detect with 90-percent confidence the largest effect that may reasonably be expected based on what is known currently about the strategy). In this case, a 20-percent reduction in right-angle crashes was assumed as this upper limit on safety effectiveness.

These sample size calculations were based on specific assumptions regarding the number of crashes per mile and years of available data. Estimates may be predicted with greater confidence or a smaller reduction in crashes will be detectable if it turns out that there are more intersection-years of data available in the after period. The same holds true if there is a higher crash rate than expected in the before period.

Table 2. Minimum Required Before Period Site-Years for Treated Sites for Crash Rate Assumptions.

Expected Percent Reduction in Crashes		95% Confidence			90% Confidence		
		A	B	C	A	B	C
All	5	1,629	738	12,773	1,141	516	8,943
	10	371	168	2,907	260	118	2,036
	20	76	34	594	53	24	416
	30	27	12	211	19	9	147
	40	12	5	92	8	4	64
Angle	5	4,163	1,892	33,060	2,915	1,325	23,146
	10	948	431	7,525	663	302	5,268
	20	194	88	1,537	135	62	1,076
	30	69	31	545	48	22	381
	40	30	14	237	21	10	166
Rear-End	5	7,114	3,212	56,203	4,981	2,249	39,349
	10	1,619	731	12,793	1,134	512	8,956
	20	331	149	2,612	232	105	1,829
	30	117	53	926	82	37	648
	40	51	23	403	36	16	282

Note: Bold denotes the minimum sample size and desirable sample size calculated for intersection-years per period.

METHODOLOGY

The EB methodology for observational before-after studies⁽⁹⁾ was used for the evaluation. This methodology is rigorous in that it accomplished the following:

- It properly accounts for regression-to-the-mean.
- It overcomes the difficulties of using crash rates in normalizing for volume differences between the before and after periods.
- It reduces the level of uncertainty in the estimates of safety effect.
- It provides a foundation for developing guidelines for estimating the likely safety consequences of contemplated strategy.
- It properly accounts for differences in crash experience and reporting practice in amalgamating data and results from diverse jurisdictions.

In the EB approach, the change in safety for a given crash type at a site is given by:

$$\Delta \text{ Safety} = \lambda - \pi, \quad (1)$$

Where:

λ is the expected number of crashes that would have occurred in the after period without strategy.

π is the number of reported crashes in the after period.

In estimating λ , the effects of regression-to-the-mean and changes in traffic volume are explicitly accounted for using safety performance functions (SPFs) relating crashes of different types to traffic flow and other relevant factors for each jurisdiction based on untreated sites. Annual SPF multipliers are calibrated to account for the temporal effects on safety of variation in weather, demography, crash reporting, and so on.

In the EB procedure, the SPF is used to first estimate the number of crashes that would be expected in each year of the before period at locations with traffic volumes and other characteristics similar to the one being analyzed. The sum of these annual SPF estimates (P) is then combined with the count of crashes (x) in the before period at a strategy site to obtain an estimate of the expected number of crashes (m) before strategy. This estimate of m is:

$$m = w_1(x) + w_2(P), \quad (2)$$

Where:

w_1 and w_2 are estimated from the mean and variance of the SPF estimate as:

$$w_1 = \frac{kP}{kP + 1} \quad (3)$$

$$w_2 = \frac{1}{kP + 1} \quad (4)$$

Where:

k is a constant for a given model and is estimated from the SPF calibration process with the use of a maximum likelihood procedure. (In that process, a negative binomial distributed error structure is assumed with k being the over-dispersion parameter of this distribution.)

A factor is then applied to m to account for the length of the after period and differences in traffic volumes between the before and after periods. This factor is the sum of the annual SPF predictions for the after period divided by P , the sum of these predictions for the before period. The result, after applying this factor, is an estimate of λ . The procedure also gives an estimate of the variance of λ , the expected number of crashes that would have occurred in the after period without strategy.

The estimate of λ is then summed over all sites in a strategy group of interest (to obtain λ_{sum}) and compared with the count of crashes during the after period in that group (π_{sum}). The variance of λ is also summed over all sites in the strategy group.

The Index of Effectiveness (θ) is estimated as:

$$\theta = \frac{\pi_{sum} / \lambda_{sum}}{1 + \left(\frac{Var(\lambda_{sum})}{\lambda_{sum}^2} \right)} \quad (5)$$

The standard deviation of θ is given by:

$$StDev(\theta) = \sqrt{\frac{\theta^2 \left(\frac{Var(\pi_{sum})}{\pi_{sum}^2} + \frac{Var(\lambda_{sum})}{\lambda_{sum}^2} \right)}{\left(1 + \frac{Var(\lambda_{sum})}{\lambda_{sum}^2} \right)^2}} \quad (6)$$

The percent change in crashes is calculated as $100(1-\theta)$; thus a value of $\theta = 0.7$ with a standard deviation of 0.12 indicates a 30-percent reduction in crashes with a standard deviation of 12 percent.

DATA COLLECTION

This section provides a summary of the data assembled for the analysis. Data were collected in two States, North Carolina, and South Carolina. These States were selected because they could provide installation locations and dates for flashing beacons that were installed in the last ten years. In both the States, flashing beacons were installed at locations where the data showed a large number of angle crashes and where drivers had difficulty recognizing the stop control

condition. All crashes that occurred within 76.25 m (250 ft) of the intersection were considered intersection-related.

North Carolina

Installation Data

The North Carolina Department of Transportation (NCDOT) provided project files from multiple districts with details about the installation of flashing beacons. For many of the sites, these files indicated whether the flashing beacon was installed overhead, on the shoulder, or on a STOP sign. They also indicated whether the flashing beacon was actuated or a standard installation.

In North Carolina, many of the evaluated flashing beacons were standard (i.e., flash 24 hours a day); however, there were also several actuated installations (i.e., flash only when a vehicle approaches an intersection). The beacons were installed either overhead or on a STOP sign.

There were limited installations of flashing beacons at three-leg, or T intersections, only three during the last 10 years, so T intersections were not included in the analysis. The analysis focused on four-leg intersections with two lanes on the major road.

Reference Sites

For many of the sites with flashing beacons, NCDOT staff had conducted a before-after safety evaluation using nearby sites for a reference group. The reference sites were provided in some of the project files. A safety evaluation was not conducted for all strategy sites, and therefore, some strategy sites had several reference sites and others had none. In addition, NCDOT also provided the reference sites used by Murphy and Hummer⁽⁶⁾ in their evaluation. For this project, all reference sites were pooled together to be used as a reference group for developing SPFs as part of the EB procedure.

Roadway Data and Traffic Data

North Carolina is one of eight States that is part of the Highway Safety Information System (HSIS). For participating States, HSIS can provide roadway characteristics and traffic information given the mileposts of the roads. The features-report module in NCDOT's Traffic Engineering Accident Analysis (TEAAS) database was used to identify the mileposts of the major and minor roads for each intersection and a query was run on the HSIS database to obtain roadway characteristics and traffic volumes. HSIS provided data on land use (i.e., rural or urban), number of lanes, lane and shoulder width, and presence of a median. The HSIS database was not able to provide major and minor road AADT for every intersection for all years. For the missing data, the research team tried to use NCDOT's AADT maps by locating each individual intersection in the map initially through GoogleTM Maps. This turned out to be a very time-consuming process. Even after the AADT map search, data were not available for every intersection for all years, especially for the minor roads. If major or minor road AADT data were missing for certain years (but available for other years) at a particular site, the missing data were filled-in using a procedure developed by Lord.⁽¹³⁾ AADT data were obtained or estimated for each reference and strategy intersection from 1990 to 2004. Tables 3 and 4 display the number of strategy and reference sites and the number of sites where minor road AADT was available.

Table 3. Four-Legged Intersections in North Carolina with both Major and Minor AADT Available.

Area Type	Reference		Strategy	
	Two-Lane	Multilane	Two-Lane	Multilane
Rural	185	2	31	4
Suburban	7	1	9	1
Urban	1	1	2	0

Table 4. Four-Legged Intersections in North Carolina with only Major AADT Available.

Area Type	Reference		Strategy	
	Two-Lane	Multilane	Two-Lane	Multilane
Rural	19	1	15	0
Suburban	8	0	5	3
Urban	11	0	2	2

Crash Data

Crash data for the reference and strategy intersections were extracted from NCDOT’s TEAAS database. Crashes may have been recorded in the crash database using alternate names. NCDOT provided alternate street names for each route, which ensured a more complete coverage of crashes when associating the crash data with each intersection.

South Carolina

Installation Data

The South Carolina Department of Transportation (SCDOT) provided installation data for 61 flashing beacons in 5 districts. Of these 61 flashing beacons, 12 were mounted on STOP signs and 49 were mounted over the intersection. The majority of the flashing beacons were installed at four-leg intersections on two-lane roads. All the flashing beacons evaluated in South Carolina are standard (i.e., flash 24 hours a day).

Reference Sites

SCDOT provided a copy of the roadway and traffic data that were collected for the Highway Performance Monitoring System (HPMS). The HPMS is a national highway information system that includes data on the extent, condition, performance, use, and operating characteristics of the Nation's highways. Using the HPMS, intersections with characteristics similar to the strategy sites were chosen for reference sites.

Roadway Data

Roadway data were collected using the HPMS database. This database provided data on the land use (i.e., urban or rural), number of lanes, lane width, presence of a shoulder, shoulder width, presence of a median, and median type for each intersection approach. Speed limit was not available for the intersections included in this study.

Traffic Data

The majority of the traffic volumes used for this study was extracted from the HPMS files. Based on communications with the SCDOT, HPMS was the best available source of traffic data for the State. These values come from a segment of roadway ranging from 0.161 to 8.05 km (0.1 to 5.0 mi) or more in length. The range is less in urban areas and greater in rural areas. Therefore, in rural areas, the volume count used to describe the volume entering the intersection may be collected from a point up to 8.05 km (5 mi) from the intersection. There are no records of where in the segment the count was actually collected.

Crash Data

SCDOT supplied crash data in two databases. One database contained crashes occurring from 1994 to 2000. The second database contained crashes occurring from 2001 to 2005. The two database system was necessary because the crash data report and some associated variables were modified in 2001. In addition, there was no threshold on reporting property-damage-only crashes prior to 1997. Starting that year, only crashes involving an injury or property damage greater than \$1,000 were reported in the system.

Based on guidance from the SCDOT, the crash milepost was not used to locate crashes. Instead, the variable "base offset distance" was used to identify crashes occurring at intersections.

Table 5 shows the number of strategy and reference sites in South Carolina. Most of the installations were at four-leg intersections along two-lane roads, which was the focus of the analysis.

Table 5. Four-Leg Intersections in South Carolina.

Area Type	Reference		Strategy	
	Two-Lane	Four-Lane	Two-Lane	Four-Lane
Rural	58	3	30	0
Urban	28	4	12	2

Summary of Data

Table 6 shows the summary of the data from the strategy sites in North Carolina and South Carolina. This table indicates a total sample of 917 intersection-years in the before period (583 in North Carolina and 334 in South Carolina) and 433 intersection-years in the after period (305 in North Carolina and 128 in South Carolina). The desired sample size was 260 intersection years to detect a 10-percent reduction in all crashes. More sites were required than originally estimated because the before-period crash rate for North Carolina and South Carolina (2.85 and 2.73, respectively) were lower than the 3.45 crashes per site-year assumed in the study design. However, since the before-period crash rates were only slightly lower and the available sample of intersection years was substantially higher than the desired sample of 260, the sample was deemed adequate to proceed with the analysis.

Table 6 also shows that the total crashes per intersection-year in the before period was lower in South Carolina, despite the higher average major and minor AADTs before the installation of flashing beacons. North Carolina experienced substantially more angle and injury/fatal crashes per intersection-year compared to South Carolina. South Carolina experienced more rear-end crashes year. The North Carolina sites experienced a much larger increase in traffic volumes between before and after periods compared to the South Carolina sites.

Information from the summary tables should not be used to make simple before-after comparisons of crashes per-site year since such an analysis would not account for factors other than the strategy that may cause safety to change between the two periods. Such comparisons are properly done with the EB analysis discussed in the following sections.

Table 6. Summary Data from North Carolina and South Carolina.

Variable	North Carolina (64 sites)		South Carolina (42 sites)	
	Before	After	Before	After
Intersection-Years	583	305	334	128
Major Road AADT (Average)	3,578	5,105	3,978	4,531
Minor Road AADT (Average)	1,540	2,074	1,938	2,192
Total Crashes	1,662	912	912	338
Crashes per Intersection/Year (Average)	2.85	2.99	2.73	2.64
Angle Crashes per Intersection/Year (Average)	1.66	1.45	1.17	1.27
Injury and Fatal (K,A,B,C) Crashes per Intersection/Year (Average)	1.68	1.58	0.94	0.89
Rear-End Crashes per Intersection/Year (Average)	0.31	0.42	0.55	0.61

DEVELOPMENT OF SAFETY PERFORMANCE FUNCTIONS

This section presents the SPFs, which were developed for the EB analysis. Generalized linear modeling was used to estimate model coefficients using PROC GLIMMIX in SAS^{®(14)} and assuming a negative binomial error distribution, which is consistent with the state of the research in developing these models. The over-dispersion parameter (k) is estimated by an iterative process assuming a negative binomial error structure. The over-dispersion parameter relates the mean and variance of the SPF estimate. The value of k is such that the smaller its value, the better a model is for a given set of data.

For both North Carolina and South Carolina, SPFs were developed for the following crash types:

- Total intersection crashes.
- Total intersection injury and fatal crashes (including K, A, B, and C).
- Total intersection angle crashes.
- Total intersection rear-end crashes.

The SPFs followed one of three forms (see equations 7 through 9). If the SPF was used for the EB analysis of treatment sites where both major and minor road AADT were available, one of the forms from equations 7 or 8 was used. If the SPF was used for the EB analysis of treatment sites where the minor road AADT was not available, the form in equation 9 was used.

$$Y = \exp\left\{a + b * \ln\left(\frac{MajorAADT}{10000}\right) + c * \ln\left(\frac{MinorAADT}{10000}\right) + d * X_1 + e * X_2\right\} \quad (7)$$

$$Y = \exp\left\{a + b * \ln\left(\frac{TotalAADT}{10000}\right) + c * \ln\left(\frac{MinorAADT}{TotalAADT}\right) + d * X_1 + e * X_2\right\} \quad (8)$$

$$Y = \exp\left\{a + b * \ln\left(\frac{MajorAADT}{10000}\right) + c * X_{\text{minorAADT_available}} + d * X_1 + e * X_2\right\} \quad (9)$$

where Y is the expected number of crashes per year of a particular type, $X_{\text{minorAADT_available}}$ is a dummy variable indicating whether minor road AADT is available or not, X_1 is a dummy variable indicating area type (rural/urban/suburban), and X_2 is a dummy variable indicating the type of traffic control (two-way versus four-way stop-control); a , b , c , d , and e are parameters to be estimated.

Safety Performance Functions (SPFs) for North Carolina

In North Carolina, SPFs were developed for all the crash types mentioned above. The following discussion illustrates the reference group used to estimate the SPFs for the different EB analyses conducted:

1. *EB analysis of rural four-leg strategy intersections where both major and minor AADT were available.* Reference group for this EB analysis included rural four-leg reference intersections where both major and minor road AADT were available.
2. *EB analysis of rural four-leg strategy intersections where minor road AADT was not available.* Ideally, for this group, an SPF should be developed with only reference sites for which minor AADT were unavailable. However, there were only 19 such reference sites—not sufficient for developing an SPF—so a reference group including all rural four-leg intersections with and without minor AADT was identified. In estimating the SPF, a dummy variable was introduced to indicate whether or not minor road AADT was available.
3. *EB analysis of suburban and urban four-leg strategy intersections where both major and minor road AADT were available.* Again, under ideal conditions, SPFs would be developed separately for suburban and urban four-leg reference intersections. However, there was not a sufficient sample of either suburban or urban reference sites to develop

separate SPFs. Neither were there sufficient sites to develop SPFs for urban and suburban intersections as a group. Therefore, a reference group that included four-leg rural, suburban, and urban intersections was used to develop an SPF with dummy variables that represented area type (i.e., suburban, urban, and rural categories). This SPF was used for urban and suburban strategy sites; for rural sites the SPF used was identified under the first bullet above.

4. *EB analysis of suburban and urban four-leg reference intersections where minor road AADT was not available.* In accordance with the discussion above, a reference group that included four-leg rural, suburban, and urban intersections with and without minor AADT was used to develop an SPF with dummy variables that represented area type (i.e., suburban, urban, and rural categories), and a dummy variable to indicate whether or not minor road AADT was available. This SPF was used for urban and suburban strategy sites where minor road AADT was not available; for rural sites where minor road AADT was not available, the SPF used was identified under the second bullet above.

The details of the SPFs developed for North Carolina are presented in tables 11 and 12 in appendix A. Parameter estimates and standard errors are provided for each variable included in the model along with the over-dispersion parameter (k) that is used in the EB analysis. In addition, two goodness-of-fit (GOF) statistics are provided for each model:

1. *Freeman Tukey R-square (R-square (FT))* based on the approach outlined in Fridstrom et al.⁽¹⁵⁾ This R-square usually tends to be higher for datasets with a large number of crashes per site. Since the number of crashes at stop-controlled intersections is relatively low, this R-square is quite low for most of the models estimated in this study.
2. *Pseudo R-square* based on the method discussed in Miaou.⁽¹⁶⁾ The Pseudo R-square is estimated based on k for the model under consideration compared with k estimated for a model with just a constant term without any independent variables. The Pseudo R-square is preferred by some researchers for datasets with low number of crashes. In general, the Pseudo R-square was higher (exceeded 0.5) for the model forms that included both Major and Minor Road AADT in North Carolina.

Tables 11 and 12 also show the annual (calibration) factors that were estimated from each of these models. The annual factor for a particular year is defined as the ratio of observed to predicted crashes for that year. Annual factors are used to account for the effect of changes in other factors over time (e.g., weather, crash reporting practices, and demography). Annual factors for all four models were estimated based on the SPFs developed for total crashes.

Safety Performance Functions (SPFs) for South Carolina

Only one set of SPFs was developed in South Carolina, because of the limited sample of reference intersections. Dummy variables were introduced for area type and type of traffic control (four-way versus two-way stop-control). Table 13 in appendix B shows the details of the SPFs developed with data from reference sites in South Carolina.

RESULTS

Based on the data, results for North Carolina and South Carolina are presented in the following sections in two parts: the first part contains aggregate results for each State and for the two States combined; the second part discusses a disaggregate analysis of the factors that may be most favorable to the installation of flashing beacons.

Aggregate Analysis

The aggregate results are shown in tables 7 through 9. All three types of flashing beacons are combined together in these results. Results that are statistically significant at the 95-percent confidence level are shown in bold. The tables show the EB estimate of the crashes expected in the after period if the beacon had not been installed, the actual number of crashes in the after period, and two measures of change. The first measure of safety effect is the estimated percent change due to the particular safety improvement strategy along with the standard error (S.E.) of this estimate; a negative value indicates an increase in crashes. A percent change that is at least 1.96 times higher than the standard error is statistically significant at the 5-percent level (equivalent to a confidence level of 95 percent); similarly, a change that is at least 1.64 times higher than the standard error is statistically significant at the 10-percent level (a confidence level of 90 percent). The second measure of safety effect is the change in the number of crashes per site year; this is the difference between the EB estimate of crashes expected in the after period and the count of observed crashes in the after period, divided by the number of site-years during the after period.

Table 7. Results for 64 North Carolina Strategy Sites—All Beacon Types Combined.

	Angle	Rear-End	Injury and Fatal (K, A, B, C)	All Crash Types and Severities
EB estimate of crashes expected in the after period without strategy	532.6	148.0	533.7	973.2
Count of crashes observed in the after period	436	127	469	894
Estimate of percent reduction in crashes (standard error)	18.3% (4.9)	14.6% (9.7)	12.2% (5.1)	8.2% (4.0)
Estimate of reduction in crashes per site-year	0.32	0.07	0.21	0.26

Note: Bold denotes results that are statistically significant at the 95% confidence level.

Intersections in North Carolina experienced a statistically significant reduction (at the 95-percent confidence level) in total crashes, angle crashes, and injury and fatal crashes. The reduction in

rear-end crashes was not statistically significant. The sites in South Carolina experienced very little change and all changes were highly insignificant. Nevertheless, the combined results in table 9 for the two States still indicate highly significant reductions in angle and injury and fatal crashes. Since North Carolina has more site-years compared to South Carolina (305 versus 128), it should not be surprising that the combined results shown in table 9 are dominated by the results from North Carolina.

The next section provides the results of a disaggregate analysis to see if these effects are more or less prominent under specific conditions. In reviewing the results of the disaggregate analysis, readers should note that disaggregate analyses are, by nature, based on smaller sample sizes than aggregate analyses, and smaller samples lead to larger standard errors and less precise results.

Table 8. Results for 42 South Carolina Strategy Sites—All Beacon Types Combined.

	Angle	Rear-End	Injury and Fatal (K, A, B, C)	All Crash Types and Severities
EB estimate of crashes expected in the after period without strategy	156.6	73.6	115.1	323.8
Count of crashes observed in the after period	162	78	114	338
Estimate of percent reduction in crashes (standard error)	-2.7% (11.7)	-3.9% (18.5)	1.8% (12.9)	-4.0% (8.2)
Estimate of reduction in crashes per site-year	-0.04	-0.03	0.01	-0.11

Note: A negative sign indicates an increase in crashes.

Table 9. Combined Results for 106 North Carolina and South Carolina Strategy Sites—All Beacon Types Combined.

	Angle	Rear-End	Injury and Fatal (K, A, B, C)	All Crash Types and Severities
EB estimate of crashes expected in the after period without strategy	689.2	221.6	648.8	1,297.0
Count of crashes observed in the after period	598	205	583	1,232
Estimate of percent reduction in crashes (standard error)	13.3% (4.6)	7.9% (8.9)	10.2% (4.8)	5.1% (3.6)
Estimate of reduction in crashes per site-year	0.21	0.04	0.15	0.15

Note: Bold denotes results that are statistically significant at the 95% confidence level.

Disaggregate Analysis

Table 10 presents the results of the disaggregate analysis. Results that are statistically significant at the 95-percent confidence level are shown in bold. Since angle crashes are the main focus of this treatment, the disaggregate analysis is focused on this crash type. The first column of the table shows the group, the States considered (North Carolina, South Carolina, or North Carolina and South Carolina), and the number of sites in that particular group. Overall, the results indicate a tendency for angle crashes to decrease following the introduction of flashing beacons except in urban areas; however, the increase in crashes in urban areas is highly insignificant. The following is a summary of the results regarding specific conditions:

- *Area type:* Flashing beacons seem to be more effective at rural and suburban locations. The sample size for suburban and urban intersections is quite low, resulting in effects that are highly insignificant; consequently, this result needs to be applied with caution.
- *Traffic control (two-way and four-way stop-controls):* There is an indication that flashing beacons may be more effective at reducing angle crashes at four-way stop-controlled intersections compared to two-way stop-controlled intersections; however, the reduction in angle crashes at four-way stop-controlled intersections is not significant.
- *Beacon type and location:* This includes standard beacons where the beacon flashes all the time and actuated beacons. Some of the actuated flashers are supplemented with a sign that reads “vehicles entering when flashing.” Standard beacons can be located overhead or on a STOP sign. There seems to be a dramatic reduction in crashes at sites with standard beacons mounted on a STOP sign. However, only five sites belong to this

category, and therefore, it is not possible to make definitive conclusions regarding beacon location.

The three types of beacons analyzed could be considered three distinct countermeasures with differing levels of safety effectiveness. There is anecdotal evidence that suggests that the overhead beacons have been interpreted as indicating a four-way stop at locations that were in fact only a two-way stop. This has caused motorists to pull out in front of the approaching vehicles because they assumed the approaching vehicle would be stopping. This has not been reported as being an issue at locations with STOP sign mounted beacons. The project team attempted to discern the different safety effects of the three types of beacons as shown in table 10. However, there was not a large enough sample size of each of the three countermeasures to produce significant results for each of the individual analysis. Because of the limited number of sites in both States, it was also not possible to look at the safety effect of combinations of factors (e.g., beacon type and area type). The effect of AADT was explored in the disaggregate analysis, but this variable does not appear to have an impact on the strategy effectiveness.

Table 10. Results of the Disaggregate Analysis for Angle Crashes.

Group (Sites)	EB estimate of crashes expected in the after period without strategy	Count of crashes observed in the after period	Estimate of percent reduction (standard error)
Rural Sites in NC and SC (76)	512.8	433	15.7% (5.3)
Suburban Sites in NC (14)	143.1	127	11.8% (10.2)
Urban Sites in NC and SC (16)	33.2	38	-12.3% (23.4)
Two-way stop in NC and SC (95)	654.9	572	12.7% (4.7)
Two-way stop in SC (31)	122.3	136	-10.4% (13.4)
Four-way stop in SC (11)	34.3	26	27.8% (20.5)
Standard Overhead in NC and SC (84)	540.6	477	11.9% (5.4)
Standard STOP Sign mounted in NC and SC (5)	16.5	7	58.2% (16.3)
All Standard in NC and SC (89)	557.1	484	13.3% (5.2)
Actuated in NC (17)	132.0	114	14.0% (9.8)

Notes: Bold denotes results that are statistically significant at the 95% confidence level. A negative sign indicates an increase in crashes.

Economic Analysis

An analysis was conducted to study the economic feasibility of this strategy. This economic analysis was accomplished by estimating the life cycle annual cost of the strategy and comparing this to the expected annual crash cost savings per intersection. In estimating the life cycle annual costs, a discount rate of 7 percent (suggested by Office of Budget and Management) was used. Crash costs were estimated from the most recent FHWA unit crash cost data for unsignalized intersections.⁽⁸⁾ Separate calculations were done for standard and actuated beacons because of the significant difference in the installation costs for these two types of beacons. The maintenance and utility costs for both beacon types range from \$400 to \$720 per year (an average of \$560). The life of a flashing beacon is at least 10 years.

Based on information from North Carolina and South Carolina, the installation costs for standard beacons, both overhead and STOP sign mounted, ranges from \$2,000 to \$27,500, with an average of about \$ 9,000. This information was used to estimate the life-cycle costs for the standard beacons as follows:

High estimates: \$27,500 installation, \$720 for maintenance; life-cycle costs = \$4,636
Average estimates: \$9,000 installation, \$560 for maintenance; life-cycle costs = \$1,841

The installation costs for actuated beacons ranges from \$10,000 to \$100,000, with an average of about \$ 23,000. This information was used to estimate the life cycle costs for the actuated beacons as follows:

High estimates: \$100,000 installation, \$720 for maintenance; life-cycle costs = \$14,958
Average estimates: \$23,000 installation, \$560 for maintenance; life-cycle costs = \$3,835

The crash-saving benefit was estimated by considering the effects on angle and nonangle crashes. Based on the results in table 10, it is assumed that these effects are similar enough for the two beacon types for the combined results in table 9 to be used. Those results show a reduction of 0.21 angle crashes per site year. The effect on nonangle crashes was deduced from the numbers for total and angle crashes. From these, an increase of 0.06 crashes per site year was obtained for nonangle crashes.

The most recent FHWA mean comprehensive costs per crash per year for unsignalized intersections are \$13,238 for rear-end and \$61,114 for angle crashes.⁽⁸⁾ The comprehensive crash costs represent the present value, computed at a discount rate, of all costs over the victim's expected life span that result from a crash. The major categories of costs used in the calculation of comprehensive crash costs included medically-related costs, emergency services, property damage, lost productivity, and monetized quality-adjusted life years.⁽⁸⁾ Angle and rear-end crashes are the two most common types of crashes at stop-controlled intersections and the overall severity of nonangle crashes is quite similar to rear-end crashes. Therefore, the cost for nonangle crashes was assumed to be equal to the cost of rear-end crashes. Using these comprehensive crash costs, the savings because of the reduced crashes was \$12,040 per site-year (0.21 of \$61,114 minus 0.06 of \$13,238).

Using the life-cycle cost estimated for standard beacons based on the higher installation and maintenance costs, this savings translates to a 2.6:1 benefit cost ratio (12,040/4,636). If a life-cycle cost of \$1,841 is used (based on average installation and maintenance costs), a 6.5:1 benefit cost ratio is achieved.

For the actuated beacons, a benefit cost ratio of 3.1:1 is achieved if average installation and maintenance costs are used. If the higher installation and maintenance costs are used, the costs exceed the benefit. Further calculations revealed that for actuated beacons that cost less than \$79,000, the benefit exceeds the costs; for installations less than approximately \$37,000, a 2:1 benefit is achieved.

SUMMARY

The objective of this study was to evaluate the safety effectiveness, as measured by crash frequency, of flashing beacons at unsignalized intersections. The study was designed to detect a 10-percent reduction in all crashes with 90-percent confidence. The study also examined the effects of flashing beacons on specific crash types including angle, rear-end, and injury and fatal crashes.

Intersections in North Carolina experienced a statistically significant reduction (at the 95-percent confidence level) in total crashes, angle crashes, and injury and fatal crashes following the installation of flashing beacons. The intersections in South Carolina experienced very little change following the introduction of flashing beacons, and those changes were highly insignificant.

CONCLUSIONS

In general, the flashing beacons at unsignalized intersections can be a cost-effective safety improvement, particularly for lower cost, nonactuated installations. The combined results indicate a significant reduction in angle crashes as well as injury and fatal crashes. Based on the conservative lower 95-percent confidence interval of the safety effect estimates, reductions of at least 4 percent for angle crashes and 1 percent for fatal and injury crashes can be expected with the installation of flashing beacons as presented in table 11. The lower 95-percent confidence limit provides a conservative estimate and the disaggregate analysis indicates situations where greater reductions may be expected. The safety effect may be larger for STOP sign mounted beacons; however, there was not a large enough sample size to make this determination. It is likely that flashing beacons will be most effective at rural intersections and locations with a high frequency of target collisions (i.e., right-angle, injury, and rear-end), particularly where driver awareness may be an issue. However, it may be necessary to use the point estimate (13-percent reduction for angle crashes and 10-percent reduction for injury and fatal crashes) when comparing various potential countermeasures, particularly when confident limits are not available for potential strategies. This way, all countermeasures are treated equally when making a cost-benefit comparison.

Table 11. Expected Crash Reductions for Flashing Beacons.

Crash Type	Point Estimate	Standard Error	Conservative Estimate
Angle Crashes	13.3%	4.6	4.3%
Fatal and Injury Crashes	10.2%	4.8	1%

Note: The conservative estimates are based on the lower 95% confidence interval and are calculated as the point estimate minus 1.96 times the standard error.

The economic analysis based on the combined results for angle and nonangle accidents from both States indicates that standard flashing beacons and the less-expensive actuated beacons are economically justified, but that a benefit cost ratio of 2:1 may not be achievable for the more expensive actuated beacons.

Future research on the impacts of the location of the beacon, overhead or mounted on a STOP sign, could provide additional insights.

APPENDIX A: SAFETY PERFORMANCE FUNCTIONS FOR NORTH CAROLINA

Table 12. SPFs for Rural Intersections in North Carolina.

Model A: $Y = \exp\{a + b*(MajorAADT/10000) + c*(MinorAADT/10000)\}$								
Model B: $Y = \exp\{a + b*(MajorAADT/10000) + (c, \text{ if } MinorAADT \text{ is available})\}$								
	Only sites where Major and Minor AADT were available (Model A)				All sites (Model B)			
	All	Angle	Injury and Fatal	Rear-End	All	Angle	Injury and Fatal	Rear-End
Variable	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)
Intercept	2.1457 (0.0738)	1.4926 (0.1034)	1.5272 (0.0930)	0.5945 (0.2048)	0.9591 (0.0790)	0.1032 (0.1123)	0.3662 (0.0979)	-0.1857 (0.1969)
ln(MajorAADT/10000)	0.4790 (0.0316)	0.3497 (0.0433)	0.4978 (0.0404)	1.3306 (0.1166)	0.7027 (0.0296)	0.5968 (0.0396)	0.6963 (0.0368)	1.4650 (0.1053)
ln(MinorAADT/10000)	0.5443 (0.0309)	0.6023 (0.0436)	0.5062 (0.0390)	0.4505 (0.0849)	-	-	-	-
Adjustment to intercept if minor AADT is available	-	-	-	-	0.1443 (0.0741)	0.2424 (0.1058)	0.1733 (0.0922)	-0.1453 (0.1751)
<i>k</i>	0.2135	0.4959	0.2635	0.5264	0.4254	0.8485	0.4540	0.6402
R-square (FT)	0.270	0.138	0.178	0.101	0.146	0.041	0.092	0.070
R-square (Pseudo)	0.740	0.562	0.703	0.813	0.464	0.278	0.459	0.720
Crashes	2712	1473	1558	265	3017	1618	1729	308
Observations (Intersection-Years)	2773	2773	2773	2773	3058	3058	3058	3058
Crashes/Intersection-Year	0.978	0.531	0.562	0.096	0.987	0.529	0.565	0.101
Annual Factor-1990	1.055				0.943			
Annual Factor-1991	0.943				0.819			
Annual Factor-1992	0.994				0.899			
Annual Factor-1993	0.849				0.815			
Annual Factor-1994	1.003				0.995			
Annual Factor-1995	1.038				1.014			
Annual Factor-1996	1.009				0.994			
Annual Factor-1997	1.044				1.022			
Annual Factor-1998	1.027				1.053			
Annual Factor-1999	0.982				1.045			
Annual Factor-2000	1.155				1.196			
Annual Factor-2001	0.989				1.055			
Annual Factor-2002	0.969				1.014			
Annual Factor-2003	0.871				0.908			
Annual Factor-2004	1.001				1.053			

Table 13. SPFs for Suburban and Urban Intersections in North Carolina.

Model A: $Y = \exp\{a + b*(MajorAADT/10000) + c*(MinorAADT/10000) + d*X_1\}$								
Model B: $Y = \exp\{a + b*(MajorAADT/10000) + (c, \text{ if MinorAADT is available}) + d*X_1\}$								
	Only sites where Major and Minor AADT were available (Model A)				All sites (Model B)			
	All	Angle	Injury and Fatal	Rear-End	All	Angle	Injury and Fatal	Rear-End
Variable	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)
Intercept (for urban)	0.6804 (0.2543)	-0.4520 (0.4238)	-0.1163 (0.3609)	-0.08543 (0.4708)	0.5019 (0.0867)	-1.0456 (0.1586)	-0.3754 (0.1178)	-0.6528 (0.1606)
ln(MajorAADT/10000)	0.4526 (0.0293)	0.3372 (0.0415)	0.4555 (0.0376)	1.0252 (0.0997)	0.6304 (0.0286)	0.5659 (0.0382)	0.6170 (0.0349)	0.9774 (0.0860)
ln(MinorAADT/10000)	0.5575 (0.0270)	0.6159 (0.0399)	0.5423 (0.0344)	0.6323 (0.0716)	-	-	-	-
Adjustment to intercept if minor AADT is available	-	-	-	-	0.3351 (0.0672)	0.4822 (0.0961)	0.3711 (0.0836)	0.1910 (0.1603)
Adjustment to intercept for suburban	2.0525 (0.2696)	2.4476 (0.4444)	2.2100 (0.3778)	1.4181 (0.5142)	0.5571 (0.1132)	1.1231 (0.1889)	0.7954 (0.1460)	0.1621 (0.2260)
<i>k</i>	0.2105	0.5316	0.2725	0.7143	0.5429	0.9879	0.6057	1.4810
R-square (FT)	0.313	0.157	0.212	0.096	0.121	0.043	0.075	-0.037
R-square (Pseudo)	0.773	0.592	0.732	0.773	0.402	0.292	0.389	0.384
Crashes	3063	1639	1749	318	3792	1911	2128	456
Observations (Intersection-Years)	2893	2893	2893	2893	3463	3463	3463	3463
Crashes/Intersection-Year	1.059	0.567	0.605	0.110	1.095	0.552	0.614	0.132
Annual Factor-1990	1.066				0.937			
Annual Factor-1991	0.986				0.883			
Annual Factor-1992	1.033				0.887			
Annual Factor-1993	0.907				0.885			
Annual Factor-1994	1.021				0.991			
Annual Factor-1995	1.024				1.031			
Annual Factor-1996	0.977				0.951			
Annual Factor-1997	1.091				1.068			
Annual Factor-1998	1.025				1.044			
Annual Factor-1999	0.965				1.007			
Annual Factor-2000	1.121				1.128			
Annual Factor-2001	0.955				0.982			
Annual Factor-2002	0.922				0.958			
Annual Factor-2003	0.873				0.890			
Annual Factor-2004	0.981				1.021			

Note: This SPF was developed using rural, suburban, and urban intersections but the intercepts for suburban and urban are only shown, because this SPF was not used for rural intersections.

APPENDIX B: SAFETY PERFORMANCE FUNCTIONS FOR SOUTH CAROLINA

Table 14. SPFs for Intersections in South Carolina.

Model A: $Y = \exp\{a + b*(MajorAADT/10000) + c*(MinorAADT/10000) + d*X1 + d*X2\}$				
Model B: $Y = \exp\{a + b*(TotalAADT/10000) + c*(MinorAADT/TotalAADT) + d*X1 + d*X2\}$				
	All (Model A)	Angle (Model A)	Injury and Fatal (Model A)	Rear-End (Model B)
Variable	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)	Estimate (S.E.)
Intercept (for urban four-way stop)	1.2717 (0.1240)	0.5438 (0.1674)	0.05202 (0.1705)	-1.0543 (0.2371)
ln(MajorAADT/10000)	0.4710 (0.0593)	0.4316 (0.0808)	0.5469 (0.0803)	-
ln(MinorAADT/10000)	0.1757 (0.0626)	0.1562 (0.0828)	0.02146 (0.0832)	-
ln(TotalAADT/10000)	-	-	-	1.1030 (0.1297)
ln(MinorAADT/TotalAADT)	-	-	-	-0.3728 (0.1327)
Adjustment for 2-way stops	-0.2755 (0.09017)	-0.2796 (0.1209)	-0.2481 (0.1235)	-0.4419 (0.1734)
Adjustment for rural	0.7946 (0.08139)	0.6746 (0.1088)	0.8162 (0.1134)	0.9324 (0.1612)
<i>k</i>	0.6194	1.0088	0.8197	1.2411
R-square (FT)	0.167	0.070	0.082	0.130
R-square (Pseudo)	0.325	0.220	0.287	0.508
Crashes	2025	964	780	369
Observations (Intersection-Years)	996	996	996	996
Crashes/Intersection-Year	2.033	0.968	0.783	0.370
Annual Factor-1994	0.801			
Annual Factor-1995	0.801			
Annual Factor-1996	1.013			
Annual Factor-1997	1.130			
Annual Factor-1998	1.172			
Annual Factor-1999	1.166			
Annual Factor-2000	1.097			
Annual Factor-2001	1.113			
Annual Factor-2002	0.999			
Annual Factor-2003	0.869			
Annual Factor-2004	0.961			
Annual Factor-2005	0.913			

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