

### Errata

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The following changes were made to the document after publication on the Federal Highway Administration website:

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Location	Incorrect Values	Corrected Values
Page number 9, Figure 12	Chart color coding was incorrect.	Corrected chart. Please find attached spreadsheet with high resolution chart.
Page number 10, Figure 14	Chart color coding was incorrect.	Corrected chart. Please find attached spreadsheet with high resolution chart.
508 text for figure 12	<b>Figure 12. Specific Foam</b> <b>Index as a function of the</b> <b>carbon content.</b> A graph showing the relationship between percent of carbon content and the foam index with three different air-entraining agents. The carbon content percent is on the x-axis ranging from 0.0 to 2.5 percent and the foam index values are on the y- axis ranging from 0.0 to 300 milliliters of air-entraining agent per 100 kilograms of cementitious materials. Blue data points and the blue trend line show data for alpha olefin sulfonate. The R <sup>2</sup> for these data	<b>Figure 12. Specific Foam</b> <b>Index as a function of the</b> <b>carbon content.</b> A graph showing the relationship between percent of carbon content and the foam index with three different air-entraining agents. The carbon content percent is on the x-axis ranging from 0.0 to 2.5 percent and the foam index values are on the y- axis ranging from 0.0 to 300 milliliters of air-entraining agent per 100 kilograms of cementitious materials. Blue squares and the blue trend line show data for alpha olefin sulfonate. The R <sup>2</sup> for these data

	is defined as 0.6311. Red data	is defined as 0.6311. Red circles and the red trend line show data for vinsol resin. This $R^2$ is		
	points and the red trend line			
	show data for vinsol resin. This			
	R <sup>2</sup> is 0.5951. Green data points	0.6416. Green triangles and the		
	and the green trend line show	green trend line show		
	resin/rosin data with an R <sup>2</sup> of	resin/rosin data with an $R^2$ of		
	0.6416.	0.5951.		
508 text for figure 14	Figure 14. Correlations	Figure 14. Correlations		
	between adsorption capacity	between adsorption capacity		
	and specific index for each	and specific index for each		
	AEA used. A graph shows the	AEA used. A graph shows the		
	correlation between foam index	correlation between foam index		
	values and values obtained from	values and values obtained from		
	fluorescence. The foam index	fluorescence. The foam index		
	values are on the x-axis,	values are on the x-axis,		
	ranging from 0.0 to 300	ranging from 0.0 to 300		
	milliliters of air-entraining	milliliters of air-entraining		
	agent per 100 kilograms of	agent per 100 kilograms of		
	cementitious materials. The	cementitious materials. The		
	fluorescence values are on the	fluorescence values are on the		
	y-axis, ranging from 0.0 to 1.6	y-axis, ranging from 0.0 to 1.6		
	milligrams of surfactant per	milligrams of surfactant per		
	gram of fly ash. The	gram of fly ash. The		
	correlations shown with data	correlations shown with data		
	points and trend lines are for	points and trend lines are for		
	three different surfactants.	three different surfactants.		
	Green data points show	Green triangles show resin/rosin		
	resin/rosin data with a	data with a correlation factor of		
	correlation factor of 0.9105.	0.8698. Red circles show vinsol		
	Red data points show vinsol	resin results with a correlation		
	resin results with a correlation	of 0.9105. Blue squares show		
	of 0.8698. Blue circles show	alpha olefin sulfonate data with		
	alpha olefin sulfonate data with	a correlation factor of 0.8758.		
	a correlation factor of 0.8758.			

### TECHBRIEF



U.S. Department of Transportation

Federal Highway Administration

Research, Development, and Technology Turner-Fairbank Highway Research Center 6300 Georgetown Pike McLean, VA 22101-2296

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### Fly Ash AEA Adsorption Capacity Estimation as Measured by Fluorescence or Foam Index

Publication No. FHWA-HRT-17-118

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This TechBrief provides an executive summary of a study that was conducted by the Federal Highway Administration's concrete laboratory at Turner-Fairbank Highway Research Center (TFHRC) related to the feasibility of using the fluorescence method to accurately and quantitatively determine the adsorption capacity of fly ash.

#### **INTRODUCTION**

Figure 1 shows a classic freeze-thaw (F-T) problem at Castlewood Canyon's structure on State Highway 83 in Colorado.<sup>(1)</sup> As shown, the F-T action has inflicted significant damage to the arch, causing the concrete to delaminate and exposing the reinforcing steel to corrosion.

One of the best ways to significantly improve concrete's ability to resist the detrimental impact of F-T action is through deliberately incorporating air-entraining agents (AEAs). When properly incorporated in fresh concrete, air-entraining admixtures stabilize small bubbles of air that are produced in concrete during mixing. These welldistributed stabilized bubbles, in turn, play an essential role in providing long term F-T durability and scaling resistance for concrete infrastructures in cold regions. Depending on concrete's degree of exposure and the nominal maximum size of the aggregate used, typically 4-8 percent total air is required to combat the F-T durability problems in concrete. Petrographic examination of the cores extracted from the Castlewood Canyon's bridge showed the total air to be less than 3 percent—way below the limit for Colorado's climate at this location, explaining the observed deterioration shown in figure 1.

Many State departments of transportation (DOTs) use fly ash as a supplementary cementitious material (SCM) in their concrete mixtures. Typically, 20–30 percent of portland cement mass is substituted by fly ash. Proper incorporation of fly ash in concrete mixtures is environmentally friendly, reduces permeability, improves durability, and overall has the potential of improving fresh and hardened concrete properties. However, one of the drawbacks of using fly ash is its adverse impact on the efficiency of the AEAs. Fly ash with high carbon content or powderactivated carbon (PAC) has the propensity to adsorb the AEAs in fresh concrete, hindering the bubbles' stabilization and potentially reducing the air content necessary to protect against damages from repeated freeze-thaw cycles. Since the carbon content of fly ashes is not commonly reported, loss on ignition (LOI) is used instead to indicate the potential effect of a fly ash on the AEA efficiency. But, the form of carbon present in the fly ash is the main contributor to AEA entrainment problems and LOI does not distinguish between different carbon forms, so fly ashes with similar LOI can present considerably different adsorption capacities.<sup>(2)</sup>

#### Figure 1. Freeze-thaw deterioration at Castlewood Canyon.<sup>1</sup>



To address the air content issues in binary or ternary mixtures, the practitioners have no other option but to increase the dosage of AEAs to compensate for the adsorption loss. However, determining the proper increase in AEA dosage is not a trivial task. To date, there are no available standardized devices that can be used to properly quantify the effect of fly ash on the AEAs dosages, so that the dosage can be adjusted. One of the widely used empirical methods of assessing the dosage rate of AEAs in mixtures containing fly ash has been the Foam Index (FI) test—a subjective test with a very high degree of variability depending on the operator's experience and the device used.

#### ADSORPTION CAPACITY MEASURED BY FLUORESCENCE

A promising method developed by Headwaters Resources, Inc. was evaluated by the Concrete Laboratory at TFHRC for its potential in measuring the adsorption capacity of fly ashes. The method uses fluorescence to indirectly but quantitatively measure fly ash adsorption. A known amount of fly ash is mixed with a solution containing a surrogate surfactant called nonylphenol ethoxylate (or P10 for short). A portion of P10 is adsorbed by the fly ash, and the rest remains in the slurry (P10 solution and fly ash). The amount of P10 that remains in the slurry is detected and quantified by fluorescence.

#### **OBJECTIVES**

The primary objectives of this study are to:

- 1- Examine the feasibility of using the fluorescence method to accurately quantify the adsorption capacity of fly ash.
- 2- Compare the results obtained from the fluorescence method with those obtained from the foam index test.

#### MATERIALS

Headwaters Resources identified and provided 10 sources of fly ash from 8 different States for this study. Table 1 shows source State, classification, calcium oxide (CaO) content, carbon content, and LOI for these fly ashes.

For the foam index tests, a type I/II portland cement and three different AEAs were used. The AEAs were selected based on previous research by Sutter, Hooton, and Scholorholtz and correspond to the following classification:<sup>(2)</sup>

- 1. Vinsol resin AEA.
- 2. Alpha olefin sulfonate AEA.
- 3. Resin/Rosin and fatty acid AEA.

Since one of the objectives of the study was to compare the results obtained with the fluorescence method to the results obtained with the foam index, foam index tests were also carried out with the P10 solution.

#### **TESTING APPROACH**

## ADSORPTION CAPACITY TESTING BASED ON FLUORESCENCE

The adsorption capacity test based on fluorescence was conducted following the procedures developed and provided by Headwaters Resources. Figure 2 shows the components of the device used in this study and also provided by Headwaters Resources.

The test methodology involved mixing distilled water with the P10 solution to create a 150-parts-per-million (ppm) P10 solution. Then, 400 mL of this solution is mixed in a magnetic stirrer for 10 minutes. Next, 20 grams of fly ash are mixed into the solution for 10 more minutes, creating a slurry. During this process, a portion of P10 is adsorbed by the fly ash, and a portion remains in solution. The slurry rests for 2 minutes to allow the suspended fly ash particles to settle, so that a solidfree slurry can be poured into the measuring chamber. An attached fluorescence probe is used to determine the concentration of the surfactant remaining in the slurry. The P10 solution fluoresces when excited by UV light.

Table 1. Fly ashes used in this study.							
ID	State	Class	CaO (%)	Carbon (%)	LOI (%)		
16045	Alabama	Class C	22.23	0.33	0.45		
16046	Ohio	Class F	3.36	1.96	2.66		
16047	Florida	Class F	6.53	1.93	3.03		
16050	Mississippi	Class F	19.99	0.84	1.01		
16052	Arkansas	Class F	10.99	0.18	0.28		
16053	Texas	Class C	23.16	0.2	0.39		
16054	Texas	Class C	22.69	0.48	0.61		
16057	North Dakota	Class F	13.12	0.27	0.29		
16058	Arkansas	Class F	14.9	NA	NA		
16066	Georgia	NA	NA	NA	NA		



The fluorescence intensity is proportional to the concentration of P10 in the slurry. Thereby, the measured fluorescence in any concentration is converted to the corresponding concentration in ppm.

The amount of surfactant adsorbed by the carbon present in the fly ash is the difference between the initial surfactant concentration and the remaining surfactant in the slurry. A total of 10 fly ashes were tested using this methodology with 4 replicates for each fly ash.

#### FOAM INDEX (FI) TEST

The FI test is used to estimate the potential effect of a specific fly ash on the air entrainment of concrete prepared with a specific cement and air-entraining admixture combination. The FI test involves the addition of AEAs (drop-bydrop) to a shaken slurry of cement, fly ash, and water and visual observation of the stability of the foam produced. The number of drops of AEA required to form a stable foam on the surface of the slurry depends on the AEA properties and the type of fly ash used. The FI is a measure of the volume of AEA added. The FI is then used as a relative measure of interaction between a specific fly ash and a specific AEA, allowing practitioners to adjust AEA dosages in a concrete mixture to maintain proper air content.

The FI test was conducted following ASTM procedure WK47452.<sup>(3)</sup> In a tightly sealed container, 8 grams of cement, 2 grams of fly ash, and 25 mL of distilled water are combined and agitated for 30 seconds using a wrist action shaker. Prior to running the FI test, the wrist action shaker was modified by extending the arm to about 6 inches (figure 3), so that the mixing intensity of the shaker would replicate that of vigorous manual handshake mixing.



As described above, an AEA is added drop by drop to the mixed slurry sample until a complete layer of foam is formed at the air-slurry interface (also called stable foam). A typical view of three stages of the air-slurry interface (no foam, foam stability in progress, foam stability achieved) is shown in figure 4.

Since the higher the AEA concentration, the faster the foam stability is achieved, the testing procedure uses AEA concentrations of 2, 6, 10, and 15 percent air-entraining admixture by volume as standard solutions, so that the foam stability can be achieved in 12–18 minutes per Note 4 of ASTM WK47572.<sup>(3)</sup>

The number of drops of AEA required to form this foam layer is converted into solution volume or foam index.

#### **RESULTS AND DISCUSSION**

#### ADSORPTION BY FLUORESCENCE TEST RESULTS

The fluorescence device measures the fluorescence of the surfactant solution

before the fly ash has been added and after adsorption has taken place. The initial and final concentrations are then used to calculate the adsorption capacity of fly ash; this is expressed in milligrams of surfactant adsorbed by a gram of fly ash. Figure 5 shows the adsorption capacity results of fly ashes with a typical standard deviation bar based on four replicates in each test. The measured adsorption capacities ranged from 0.26 mg/g to 1.52 mg/g.

## Figure 4. Typical view of three stages of the air-slurry interface.



Figure 6 shows the coefficient of variation (CoV) based on four replicate tests as a function of the measured adsorption capacity of the fly ashes. Fly ashes with





Figure 6. Adsorption capacity results v. coefficient of variation based on four replicate tests for each data point.



15 percent. However, two of the fly ashes (20 percent of the tested samples) whose adsorption capacities were below 0.5 mg/g, showed CoVs of 31 percent and 43 percent.

This suggests the precision of the device needs improvement to evaluate fly ashes with an adsorption capacity of 0.5 mg/g or below. On the other hand, fly ashes with higher adsorption capacity are the ones that pose the most concern and require AEA dosage to be adjusted for proper air content in concrete. Fly ashes with low adsorption capacity may have lesser air problems with an air-entraining admixture in concrete.

Figure 7 shows that the adsorption capacity of fly ashes is, to some extent, proportional to its carbon content; but the carbon content and the form of available carbon are both important, and these do not necessarily correlate with one another. As a result, carbon content may not be a good indicator of possible air entrainment problems.





As shown in figure 8, no relation between adsorption capacity and LOI could be found for the fly ashes tested. LOI proved an unreliable way to identify fly ashes that may adversely impact the efficiency of AEA, as previously shown by others.<sup>(2)</sup>

At present, the fluorescence device can measure the adsorption capacity of fly ash using the P10 as surrogate surfactant. However, once fully evolved, it should have the potential to be used with any available air entraining admixtures in the market.

#### FOAM INDEX TEST RESULTS

Figure 9 shows the foam index test results expressed as the specific foam index

(SFI) with a typical standard deviation bar based on three replicate tests. SFI is expressed as a dose of an undiluted airentraining admixture in mL per 100 kg cementitious material, which is relevant to air-entraining admixture dosage rate. As observed, the SFI can vary significantly for the same fly ash and portland cement, depending on the AEA used. This confirms the need to determine the adsorption capacity of a specific cementitious system with a specific AEA. The SFI may also vary with the fly ash content, but since the test methodology uses a constant fly ash volume, this effect was not evaluated in this study. The most significant absolute SFI variations were obtained using fly ashes 16046, for which

the vinsol resin AEA SFI was 134 mL AEA/100Kg and the alpha olefin sulfonate AEA SFI was 270 mL AEA/100Kg; and fly ash 16050, for which the vinsol resin AEA SFI was 138 mL AEA/100Kg and the alpha olefin sulfonate AEA SFI was 269 mL AEA/100Kg.

Since the index test is a visual rating system, the foam stability observed by one operator may not be the same as the one observed by another operator. Figure 10 shows the foam stability observations from two operators using the same samples. The SFI was similar between the two operators except when SFI values were higher than 200 mL per 100 kg of cementitious material as shown in figure 10. Both operators were American Concrete Institute (ACI) certified with more than 5 years of testing experience.

The effect of the AEA concentration was also investigated: using a high-strength solution tends to overestimate the result as compared to a low-strength solution even when the stable foam is formed within the time limit of 12-18 minutes. Figure 11 shows the SFI results tested with 6 and 10 percent strength solutions (medium and high concentrations, respectively) compared to the same fly ashes tested with 2 percent strength



Figure 10. Specific Foam Index observations between two operators. 300 Foam Index, mL AEA/100 kg CM 250 200 Operator #1 150 100 50 0 0 50 100 150 200 250 300 Operator #2 Foam Index, mL AEA/100 kg CM Alpha olefin sulfonate Vinsol resin Resin/Rosin LOE

solution (low concentration). As seen in the figure, the SFI results between the low and the medium to high strengths are plotted mostly over the line of equality (LOE), indicating a good estimation of AEA adsorption regardless of the solution strength. Looking at the data more closely, the SFI results for the resin/rosin and fatty acid AEA were consistently over the LOE. This suggests a systematic overestimation due to the use of higher strength solutions. So, the effect of the solution's strength on the SFI seems to be dependent on the AEA used. Therefore, the results of the foam index should be interpreted carefully when obtained using high-strength solutions.

The relationship between SFI and the carbon content is relatively good (see figure 12), considering the subjectivity and variability of the foam index test and that the carbon content does not differentiate the form of carbon present. In addition, it is clear that the relationship between SFI and carbon content is different for each AEA.

When using P10 solution, foam stability could not be maintained over 15 seconds indicating that it should not be used for foam index testing. Figure 13 shows a typical foam formation with the P10 surfactant solution.



Figure 12. Specific Foam Index as a function of the carbon content.



R<sup>2</sup>: coefficient of determination

# Figure 13. Typical foam formation of P10 solution.



#### **CORRELATIONS**

Although adsorption measured by fluorescence and the foam index are different approaches for evaluating the adsorption capacity of fly ash in the aqueous solution, figure 14 shows good correlations ( $R^2$ >0.86) between them. Nevertheless, it is clear that the relation between each AEA and adsorption measured by fluorescence is different.

#### SUMMARY AND RECOMMENDATIONS

This study examined the feasibility of using fluorescence-based technology to quantitatively measure the adsorption capacity of fly ashes and compared the results obtained by fluorescence with those obtained from the foam index test. The fluorescence-based device quantifies the adsorption capacity of a standard solution (P10) at a specific concentration (150 ppm) by fluorescence. The foam index test relies on the visual evaluation of the operator-i.e., subjective evaluation-to estimate the adsorption capacity of a specific AEA using a specific portland cement and fly ash combination. Although the foam index test evaluates specific combinations of AEA and cementitious materials that are to be used for the job mixture, this still relies on a fixed fly ash content and not necessarily the content proposed in the job mixture design.



The observations presented herein reflect the materials used in this research, especially the fly ashes, which had a LOI ranging between 0.29 and 3.03 percent, much lower than the maximum allowed by ASTM C618.<sup>(4)</sup> The behavior of higher LOI fly ashes may vary from those presented in this study.

Neither carbon content nor LOI seemed to be able to reflect the adsorption behavior of the fly ashes, because some forms of carbon are more prone to adsorbing AEA than others, and neither carbon content or LOI differentiate the form of carbon present. Some observations regarding the use of adsorption measured by fluorescence to measure fly ash adsorption capacity include:

- Fly ash containing high iron content appears to cause acceleration of the magnetic stirrer bar during the mixing process. A mechanical stirrer with fixed speed may solve this issue.
- The initial concentration (IC) with 150 ppm P10 standard solution deviated more than 5 percent from the targeted value.
- The repeatability of the method to measure adsorption capacity using fluorescence, in terms of COV, was found to be mostly below 15 percent for fly ashes for measured adsorption capacity above 0.5 mg/g. On the other hand, when fly ashes with adsorption capacity lower than 0.5 mg/g were tested, the COV was unacceptably high, showing that this methodology still needs to be improved.
- Currently, the fluorescence-based device to measure adsorption capacity is based on the P10 standard solution; other commercial air-entraining admixtures could

potentially be used with different optic filters.

These are some additional observations regarding the foam index test:

- When using a wrist action shaker apparatus, the arm needs to be modified to mimic hand shake mixing.
- Specific Foam Index is a better expression to use than the foam index, because it is related to a specific air-entraining admixture and its dosage rate.
- Operator-to-operator variability on visual rating may be attributed not only to level of training, but also the adsorption capacity of the specific fly ash, portland cement system, and the AEA used.
- Reliability of the foam index test should be interpreted carefully when high-strength solutions are used. The effect of the solution strength seems to differ from one AEA to another.
- A good correlation ( $R^2 > 0.86$ ) was • found between adsorption capacity and the specific foam index. The relationship between the results obtained by the two methods is specific to each individual airentraining admixture. This indicates that the adsorption method results do not reflect the behavior of any particular system (combination of portland cement, fly ash, and AEA). The tests can be useful tools only when comparing potential adsorption of different fly ashes and not for evaluating the potential behavior of a fly ash-AEA combination.

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#### DISCLAIMER

Certain commercial products are identified in this paper to specify the materials used and procedures employed. In no case does such identification imply endorsement or recommendation by the Federal Highway Administration nor does it indicate that the products are necessarily the best available for the purpose.

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**Researchers**—This study was performed by H. Kim and M. Nicolaescu, SES Group and Associates and A. Ardani, FHWA.

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